

# Innovative Approach to the Generation of Reverberation Time Series and Echo Detection Algorithm

S. Balayya

Assistant Professor, Department of ECE, Welfare Institute of Science Technology and Management,  
Visakhapatnam, Andhra Pradesh, India

**Abstract**— An approach to the generation of time series and echo detection algorithms is presented and demonstrated. The SONAR system transmits pulses of acoustic signals to detect the target under the sea surface. The transmitted waves are reflected off objects in their paths, creating echoes that return to the vessel and are picked up by the sonar equipment. The received signal consists of echo signal, reverberated signal and noise signal. Echo is made when sound hits the target and bounces back. Reverberation is delayed repetition of sound reflected from the sea surface and bottom. The desired echo signal and reverberation have same characteristics, because of this it is very difficult to separate echo from the reverberation. The computer simulated reverberation time series are of high quality, in that they are accurate representations of those which would result from an actual sonar system(transmit/receive and horizontal/vertical beam patterns; pulse type, shape, length, and power; frequency and sampling rate),platform(speed and depth),and environment(wind speed and direction, backscattering strengths, and propagation loss).The time series approach utilizes recent developments in linear spectral prediction research in which the spectra of stochastic process are modelled as rational functions and algorithms are used to efficiently compute optimal estimates of coefficients which specify the spectra. The approach taken in this paper is to detect echo signal in two steps . In the first part the expected reverberation spectra for all beams are predicted. In the second part time series is generated from the expected spectra.

**Keywords**— Active sonar, Reverberation, Autoregressive model, Reverberation spectrum, pre-whiten

## I. INTRODUCTION

**S**ONAR is an acronym for sound navigation and ranging .sonar is a system that uses transmitted and reflected underwater sound waves to detect and locate submerged objects or measure the distance of underwater target. In sonar, the sound was generated by projector, through the sea to the target and returned as echoes to a hydrophone which converts these acoustic signals to electric signals. The electric output of hydrophone is amplified to a control or display device to accomplish the purpose for which the sonar system was intended. A sonar systems, equipments and devices are said to be active when the sound is purposely generated by one of the system component called the projector. The sound waves generated by the projector travel through the sea to the target and are returned as sonar echoes to a hydrophone which converts sound into electricity. The simplest active sonar w have an omni directional projector and hydrophone .Its detection performance is given by the allowable two way propagation loss i.e. from projector to target and back to hydrophone. Practical active sonar will have directional transmit and receive arrays.

Sonar Reverberation (and radar clutter) has been modeled in a variety of ways and for a diversity of applications. Expected reverberation power (intensity) level models are perhaps the most common. In these, the expected reverberation power level at the input, output, or some intermediate point in the sonar (radar) system is estimated as a function of the environmental and system parameters. The models are useful in evaluating system performance for signal processing approaches which depend primarily upon power level, such as single beam energy detectors and matched filters. As systems increase in complexity, making use of multiple beams, platform motion, and complex coherent signal processing, power level alone is an insufficient parameter to describe the interfering effects of reverberation..

## II. TIME SERIES MODELING

Recent developments in linear spectral prediction (UP) techniques allow stochastic processes to be modeled in a straightforward manner. Common time series models of sampled stochastic processes, which are basic to many LSP techniques, include autoregressive (AR), moving average (MA), and autoregressive moving average (ARMA) processes. These processes can be realized as the outputs of linear digital filters driven by white noise processes, where the filter transfer functions have all-pole, all-zero, and pole-zero realizations for **AR**, **MA**, and **ARMA** processes, respectively. The digital filters can be implemented as recursive infinite impulse response (**IIR**) filters for **AR** and **ARMA** processes, and as a transversal finite impulse response (**FIR**) filter for an **MA** process. If the stochastic process to be modelled is nonstationary: but quasi-stationary, the digital filter realization is time varying, with time-varying poles and/or zeros.

### A. Autoregressive Process

In an auto regressive model of order p, the value  $\overline{x_n}$  of the complex stochastic process at time n given as a linear combination of past values and a random input  $\xi_n$ , such that

$$\overline{x_n} = -\sum_{k=1}^p b_k \overline{x_{n-k}} + \sigma \xi_n \quad (1)$$

Where  $\xi_n$  is a complex white noise process with zero mean and unity standard deviation. The system transfer function  $H(Z)$ , between input and output is represented in terms of model parameters as an all pole function.

$$H(z) = \frac{\sigma}{1 + \sum_{k=1}^p b_k z^{-k}} \quad (2)$$

The poles of  $H(Z)$  are the zeros of the polynomial in the denominator and the number of poles p is referred to as the model order. The discrete power density spectrum is

$$p_m = \frac{\sigma^2 \Delta t}{\left| 1 + \sum_{k=1}^p b_k e^{-j2\pi m k / M} \right|^2} \quad (3)$$

Where  $\Delta t$  is the sampling interval and  $p_m$  is the power at radial frequency. The problem of modeling an arbitrary stochastic process  $\{x_n, n = \dots, -1, 0, 1, \dots\}$  as an AR process reduces to the selection of the model parameters. The manner in which they are selected will depend on a priori information about  $\{x_n\}$ . A standard formulation is to select the model parameters such that the linear estimate of the process  $\{x_n\}$  at the present time n, given the past p values of the process  $\{x_{n-k}, k = 1: 2, \dots, p\}$ , is best in a least squares sense. That is, defining the linear estimate of order p as

$$x_n^* = -\sum_{k=1}^p b_k x_{n-k} \quad (4)$$

the parameters are selected such that the estimation error is minimized in a mean square sense

$$\min_{\{a_k\}} E\{\varepsilon_n^2\} = \min_{\{a_k\}} E\left\{\left(x_n + \sum_{k=1}^p b_k x_{n-k}\right)^2\right\} \quad (5)$$

This is the digital Wiener optimal one-step prediction filtering problem, and it leads to the specification of the  $\{b_k, \sigma\}$  as the solution of the normal equations

$$\rho_{in} = -\sum_{k=1}^p b_k \rho_{i-k,n} \quad i=1,2,\dots,p \quad (6a)$$

$$\rho_{on} = -\sum_{k=1}^p b_k \rho_{kn} + \sigma^2 \quad (6b)$$

where  $\rho_{i-k,n}$  is the time-varying autocorrelation function of the nonstationary process.

$$\rho_{i-k,n} \triangleq E\{x_{n-k} x_{n-i}^*\} \quad (7)$$

If the spectrum (which in general is time-varying) of the process is known, then the auto-correlation function can be found by inverse Fourier transformation and the parameters  $\{b_k, \sigma\}$  evaluated. If the spectrum is not known, but one has the past p values of the process, as in the above Wiener filtering formulation, then the auto covariance function can be used as a local estimate of the autocorrelation function.

$$\phi_{i-k,n} \triangleq \begin{cases} \sum_{j=n-p-i}^{n-1-k} x_{j-k} x_{j-i}^*, & i < k \\ \sum_{j=n-p-j}^{n-1-i} x_{j-k} x_{j-i}^*, & i > k \end{cases} \quad (8)$$

The auto covariance function can then replace the autocorrelation function in the normal equations. With this replacement, are known as the Yule-Walker equations and will be referred to in this way in this paper, regardless of whether the auto covariance or autocorrelation functions are used in them. A variety of ways to solve the Yule-Walker equations are available. We will use the Levinson-Durbin approach. Having solved for estimates of the model parameters in this way, one can evaluate the spectral estimate or the linear estimation filter transfer function &z) by using the parameter estimates in expressions (3) and (2), respectively.

The filter will produce a statistical realization of the process {x} when driven by white noise. The spectral estimate is sometimes referred to as the maximum entropy spectral estimate.

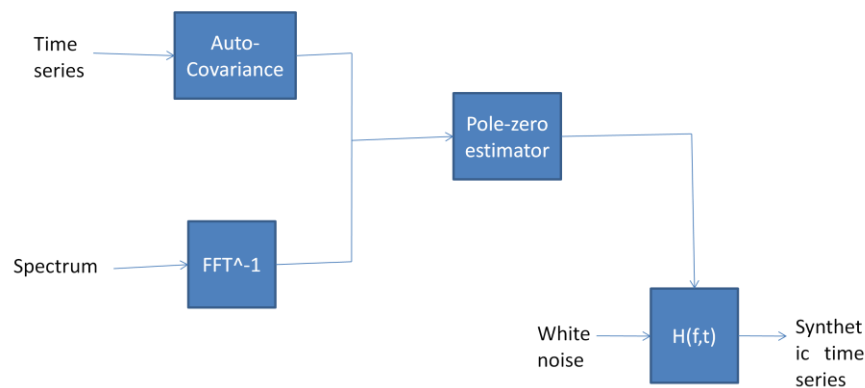


Fig-1. Linear Spectral Prediction Approach To Modeling Stochastic Quasi-Stationary Coherent Time Series.

The Levinson-Durbin algorithm is utilized to solve the Yule-Walker equations to obtain the optimal set of non stationary poles, or more precisely, the optimal set of non stationary filter coefficients for each beam.

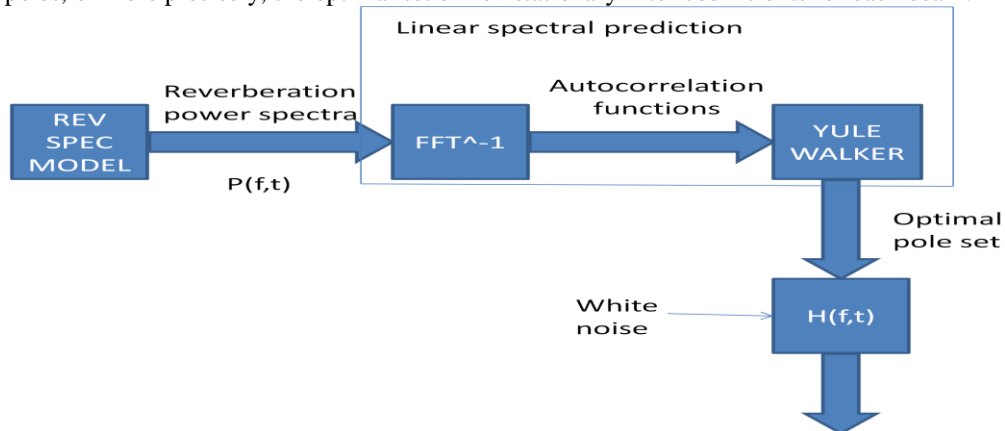


Fig-2. Processing Flow Of Reverberation Simulation Model.

The generation of coherent reverberation which is correlated between beams and overlapping spectra is illustrated in Fig.3 ,where Ha, Hb, ..., Hn,, represent transfer functions of the linear filters associated with beams, a, b, ...,n, respectively.

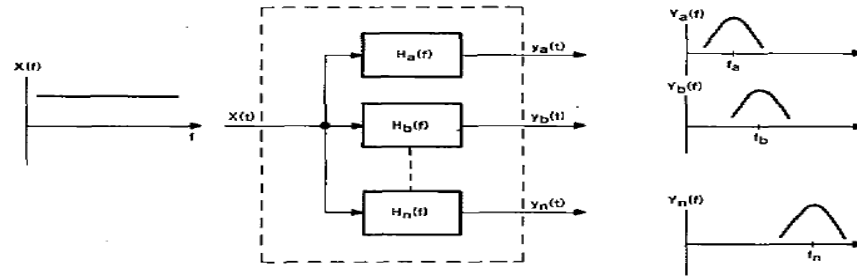


Fig-3. Parallel Structure Of Coherent Multiple-Beam Time Series Filter

### III. REVERBERATION SPECTRUM MODELING

The generation of a time series based on the existence of a spectrum was discussed. Here, an approach to generating the expected spectrum for sonar reverberation as a function of pertinent sonar system parameters and environmental conditions is presented. The approach is a numerical evaluation scheme based on a spatial grid approach of Ackerman for a general formulation of reverberation developed by Faure, Ol'shevskii and Middleton. This leads to the computation of surface, volume, and/or bottom reverberation spectra and Dower levels as functions of:

- transmit signal waveform and power level,
- spreading and absorption propagation losses,
- backscattering strength,
- transmit and receive beam patterns,
- sonar platform-ocean geometry, and
- sonar and scatter motion.

Although the formulation can be extended to relax some of the following , intrinsic assumptions include:

- primary scattering only,
- iso-sound-speed ocean,
- direct propagation path,
- narrow-band transmit signals,
- back scattering is from a large number of randomly distributed weak discrete scatters,
- radial velocity distribution of scatters is spatially uniform.

In order to make the analysis tractable we make the following assumptions:

- reverberation is a zero-mean random process;
- many scatterers simultaneously contribute to the reverberation producing a Gaussian signal (i.e., central limit theorem);
- the transmitted signal and resultant reverberation are narrow Band (i.e., the signal bandwidth is a small fraction of the carrier frequency);
- the sonar transmitter and receiver are colocated;
- scatterer radial velocities are independent and identically distributed Gaussian random variables for all volume and boundary scattering elements;
- scatterer cross sections are independent of spatial position;and
- reverberation can be considered stationary over short intervals of time (i.e., quasi-stationarity

#### A. Faure, Ol'shevskii And Middleton Formulation:

The power density spectrum  $P_f(f, r)$  of the reverberation envelope at the receiver input from scatters at range  $r$  and frequency  $f$ , letting  $*$  designate the convolution operations given by

$$P_f(f, r) = \sigma^2(r) Y_f(f, r) * |S_{Tf}(f)|^2 * D_f(f) \quad (9)$$

Where

$\sigma^2(r)$  = Total reverberation power from scatters at range  $r$ ,

$Y_f(f, r)$  = Sonar motion envelope (power density) spectrum resulting from sonar motion and stationary (non moving) scatters at range  $r$ ,

$$\int_{-\infty}^{\infty} Y_f(f, r) df = 1 \quad (10)$$

$|S_{Tf}(f)|$  = Transmit signal envelope (energy density) Spectrum,

$$\int_{-\infty}^{\infty} |S_{Tf}(f)|^2 df = 1 \quad (11)$$

$D_f(f)$  = Scatter motion spectrum resulting from random motion of the scatters.. Since it is a probability function.

$$\int_{-\infty}^{\infty} D_f(f) df = 1 \quad (12)$$

The terms  $\sigma^2$ ,  $Y_f$  and  $D_f$  depends on whether the reverberation is from volume, surface or bottom scatters. The reverberation power levels are given by

$$\sigma_v^2(r) = \frac{p_0^2 c T s_v 10^{-2\alpha r}}{2r^2} \int_{\theta_B}^{\theta_S} \int_0^{\pi} b_{TR}(\theta, \psi) d\psi d\theta \quad (13)$$

$$\sigma_s^2(r) = \frac{p_0^2 c T s_s 10^{-2\alpha r}}{2r^3} \int_0^{\pi} b_{TR}(\theta_s, \psi) \cos \theta_s d\psi \quad (14)$$

$\sigma_B^2(r)$  = same as  $\sigma_s^2(r)$ , except  $s_B$  and  $\theta_B$  replace  $s_s$  and  $\theta_s$  respectively. (15)

Where

$p_0^2$  = transmit source mean square pressure,  
C = speed of sound in water (m/s)  
T = time duration of transmit signal (s),  
r = range from mono static sonar to center of set of discrete scatterers (m),  
 $\alpha$  = absorption loss ,

$s_v, s_B, s_s$  = volume (m-3), surface (m<sup>-1</sup>) bottom (m-2) backscattering strength, respectively,

$b_{TR}(\theta, \psi)$  = transmit-receive product power beampattern.

$\psi$  = azimuthal angle (rad),

$\theta$  = elevation angle (rad),

$\theta_s$  = sin<sup>-1</sup>(z/r) = elevation angle to surface at range  $r$  and sonar depth  $z$  (rad),

$\theta_B$  = sin<sup>-1</sup>(z<sub>B</sub>-z/r) = elevation angle to bottom, at range  $r$  and sonar vertical distance above bottom of (z<sub>B</sub> - Z) (rad).

The transmit-receive beam pattern is further defined by

$$b_{TR}(\theta, \psi) = [b_T(\theta, \psi) + b_T(\theta, -\psi)] \cdot [b_R(\theta, \psi) + b_R(\theta, -\psi)] \quad (16)$$

Where

$b_T(\theta, \psi)$  = transmit power beam pattern

$b_R(\theta, \psi)$  = receive power beam pattern

$$S_s = 10 \log s_s$$

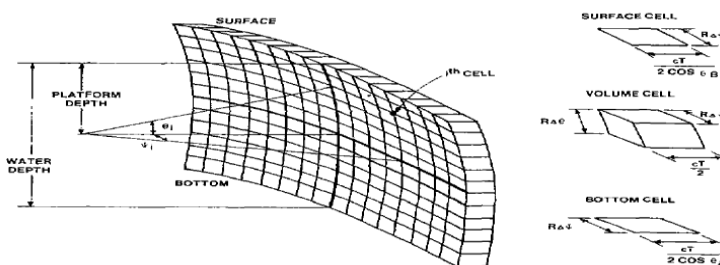
$$= 3.3 \beta \log(\theta_s/30) - 42.4 \log \beta + 2.6$$

$$\begin{aligned} S_B &= 10 \log s_B \\ &= 10 \log(\sin^2 \theta_B) - 27. \end{aligned} \quad (19)$$

$$Y_{vf}(f, r) = F \left\{ \frac{\int_{\theta_B}^{\theta_S} \int_0^{\Pi} b_{TR}(\theta, \psi) \exp\left(\frac{j4\Pi v_0 T}{\lambda}\right) d\psi d\theta}{\int_{\theta_B}^{\theta_S} \int_0^{\Pi} b_{TR}(\theta, \psi) d\psi d\theta} \right\} \quad (20)$$

$$Y_{sf}(f, r) = F \left\{ \frac{\int_0^{\Pi} b_{TR}(\theta_S, \psi) \exp\left(\frac{j4\Pi v_0 T}{\lambda} \cos \theta \cos \psi\right) \cos \theta_b d\Psi d\theta}{\int_0^{\Pi} b_{TR}(\theta_S, \psi) \cos \theta_S d\Psi} \right\} \quad (21)$$

$$Y_{Bf}(f, r) = \text{same as } Y_{sf}(f, r) \text{ except } \theta_s \text{ replace } \theta_b. \quad (22)$$



The power density spectrum  $Pf(f, \mathbf{r})$  of the reverberation envelope given by (9) is evaluated numerically dividing space into a set of cells, as illustrated in Fig. 6. The ocean is divided into spherical shells which represent the portion of the ocean that is ensonified by the signal wavefront at particular instants of time after transmission (and corresponding ranges).

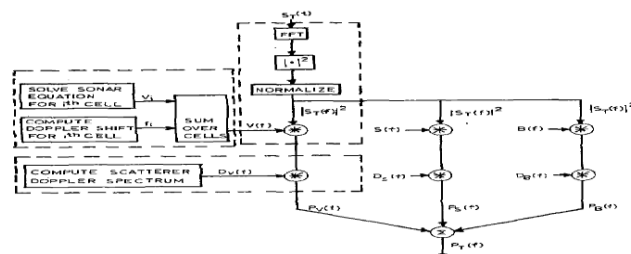


Fig- 5. Reverberation Spectrum Model

#### IV. DETECTION OF ECHO SIGNAL IN REVERBERATION BACKGROUND

Reverberation is caused by seabed, sea surface and the inhomogeneity of the granule in the seawater. As an noise, reverberation can influence the detection performance of target echo and cause some serious problems to active sonar. Due to the fact that reverberation and target echo are correlative and their spectrums are close, how to restrain reverberation is a problem necessary to be solved for active sonar. In order to restrain the reverberation signal we are using pre-whiten method here.

##### A. Pre-whiten method

The principle of this method is that an AR model is established from reverberation and then a whiten filter is designed using the power spectrum of this model. Reverberation data is considered as Gaussian color noise. And the spectrum transformations between adjacent data segments are not obvious. The rationality of this hypothesis has been verified. The performance of this method is nicer even echo-to-reverberation ratio is comparative low. On the premise of this hypothesis, a method using all-pole pre-whiten filters is proposed based on AR model at first. Then, based on this model, order partition algorithm is brought forward in detail.

The AR model of reverberation data is shown in equation

$$r(n) = -\sum_{i=1}^p a_i r(n-i) + w(n) \quad (23)$$

where  $w(n)$  is a Gaussian white noise with an average of 0,  $\{a_1, a_2, \dots, a_p\}$  are estimated using the adjacent segment data. And its power spectrum is shown in equation (2).

$$s(w) = \frac{\sigma^2}{\left| 1 + \sum_{i=1}^p a_i e^{-j\omega i} \right|^2} \quad (24)$$

When the parameters  $a_i$  of this AR model have been estimated, the system function of pre-whiten filter is as follows:

$$H(z) = \frac{1}{1 + \sum_{i=1}^p a_i z^{-i}} \quad (25)$$

Output data  $y(n)$  is obtained by data  $x(n)$  passing the above system function

$$y(n) = x(n) * z^{-1}[H(z)] \quad (26)$$

##### B. Order Partition Pre-Whiten Algorithm

Order partition pre-whitens algorithm means that the sampled reverberation data is processed according to time order.

Firstly, reverberation data is partitioned into several segments. Supposing that the echo signal  $s(n)$  is included in the signal  $x(n)$  which is received by hydrophone during the observation time  $T$ . The pulse width of  $s(n)$  is  $T_p$ . Data  $x(n)$  is partitioned into several segments and the width of each segment is

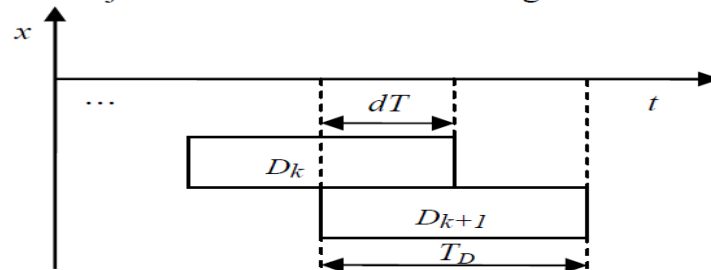


Fig 6. Sketch Map Of Data Partition

Firstly, reverberation data is partitioned into several segments. Supposing that the echo signal  $s(n)$  is included in the signal  $x(n)$  which is received by hydrophone during the observation time  $T$ . The pulse width of  $s(n)$  is  $T_p$ . Data  $x(n)$  is partitioned into several segments and the width of each segment is  $T_D$  as manifested in Fig.1, where  $dT$  denotes offset between the adjacent  $k$ th and  $k+1$ th data segments. The following conditions should be satisfied when partitioning the data into several segments:

(1) The width of each data segment should be equivalent to the usable signal  $s(n)$  in order to satisfy the requirement of local stationarity.

(2) To ensure that the echo signal  $s(n)$  is fully included in one segment, the width of  $s(n)$  should be smaller than each data segment. The following inequation should be satisfied:

$$T_D > T_p \quad (27)$$

(3) To ensure that the echo signal  $s(n)$  is situated in the next adjacent data segment when  $s(n)$  is not completely included in a certain segment, following inequation should be satisfied:

$$dT \leq T_D - T_p \quad (28)$$

According to the actual situation, the width of each data segment is double of the usable signal and the data overlapping rate is  $1/2$ .

$$T_D = 2T_p \quad (29)$$

$$dT = 1/2(T_D) \quad (30)$$

Secondly, the AR model of the  $k$ th data segment is established. In the method, the system function of the prewhiten filter which is based on the  $k$ th data segment for the  $k+1$ th data segment is as follows:

$$H_k(z) = \frac{1}{1 + \sum_{i=1}^{pk} a_{k,i} z^{-i}} \quad (31)$$

Lastly, the output data  $y_{k+1}(n)$  is obtained by passing data  $x_{k+1}(n)$  through above system function:

$$y_{k+1}(n) = x_{k+1}(n) * z^{-1}[H_k(z)] \quad (32)$$

The flow chart of order partition pre-whiten algorithm is shown in below figure.

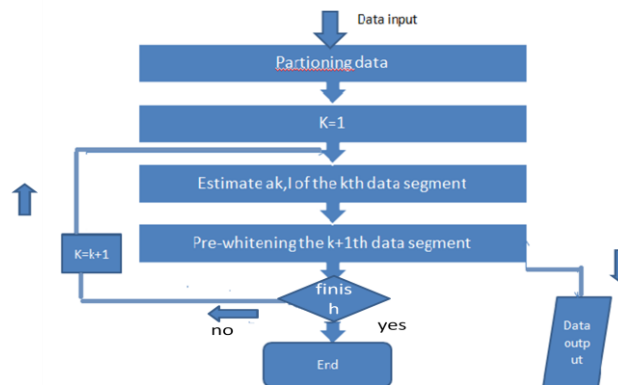


Fig 7:Flow Chart Of Order Partition Pre-Whiten Algorithm

## V. SIMULATIONS AND RESULTS

The reverberation power spectrum using faure,olshevskii, and middleton formulation is obtained and the according to the block diagram and the time series using autoregressive model is obtained.



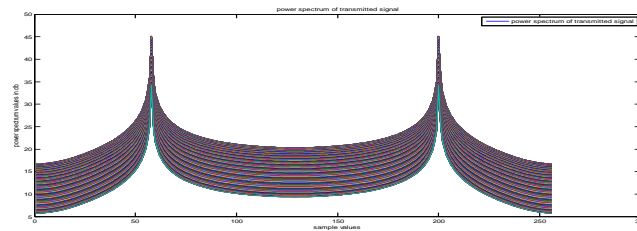


Fig-8 Transmitted Signal Power Spectrum

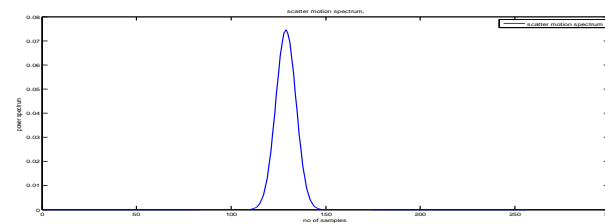


Fig-9. Scattering Motion Spectrum

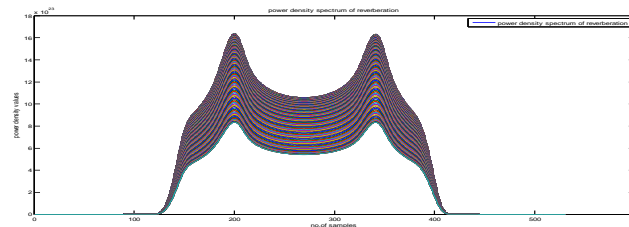


Fig-10. Power Density Spectrum Of Reverberation

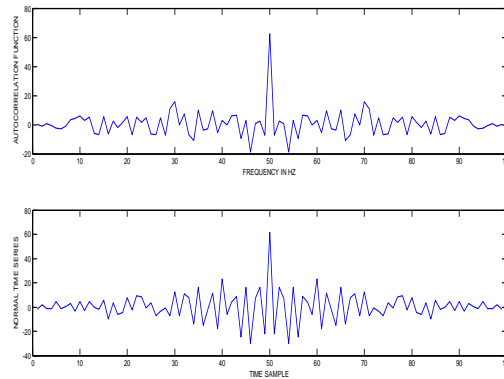


Fig-11. Time Series from autocorrelation function

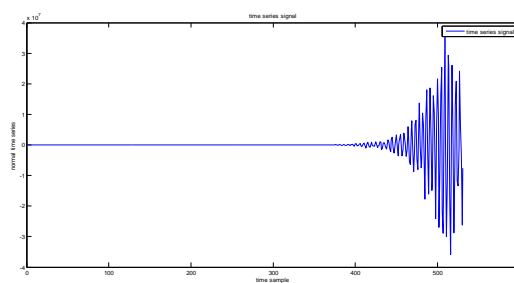


Fig-12. Time Series from the reverberation spectra

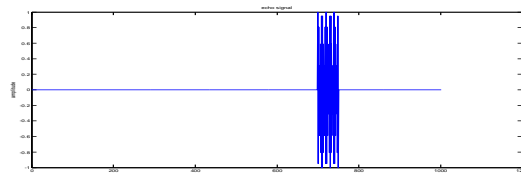


Fig 13: Echo Signal

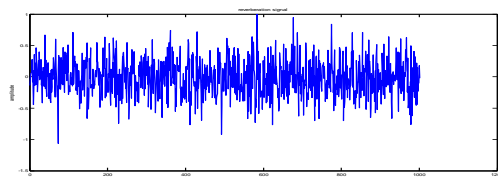


Fig 14: ReverberationSignal

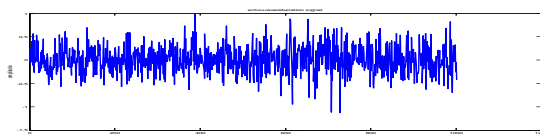


Fig 15 : Echo+Reverberation Signal

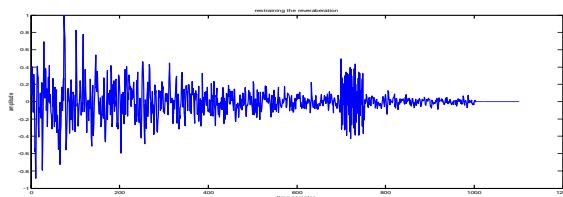


Fig 16: Restraining The Reverberation Signal

## II. CONCLUSION

This paper describes the approach to the numerical generation of reverberation time series and echo detection algorithm. on the premise of local stationary of reverberation, a method using all pole partition pre whiten filters which is based on AR model is proposed. The simulation results indicate that this method is effective even in the background of low echo to reverberation ratio of input. Moreover, the order partition algorithm is the better approach for detecting the echo signal in reverberation background.

## REFERENCES

- [1]. S. G. Chamberlain and J. C. Galli, "A Model for Numerical Simulation of Non stationary Sonar Reverberation Using Linear Spectral Prediction," IEEE journal of oceanic engineering VOL. OE-8, NO. 1, Jan. 1983, pp 21-36.
- [2]. H. Weinbeg, "Navy interim surface ship model(NISSM) 11," Naval Underwater Svstems Ctr., New London, CT. NUSC Tech. Publ. 372 and NUSC Tech. Rep. 4527, 1973.
- [3]. P. C. Etter and R. S. Plum, "A survey of underwater acoustic models and environmental acoustic data banks." Naval Anti- Submarine Warfare Syst.Proj. Office, Dept. of Navy, Washington DC, ASWR Tech. Rep.80-1 15,1980.
- [4]. C. L. Ackerman and R. L. Kesser. "Reverberation spectrum model for matched filter homing systems." Pennsylvania State Univ. Applied Research Lab, Tech. Memo. File TM73-285, Dec. 4, 1973.
- [5]. P. Faure, "Theoretical model of reverberation noise," J. Acoust.Soc.Amer.,vol. 36. no. 2. pp. 259-266.Feb. 1964.
- [6]. V. V. Ol'shevskii, Characteristics of Sea Reverberation. English translation by V. M. Albers. New York: Consultants Bureau,1967.
- [7]. D. Middleton. "A statistical theory of reverberation and similar first order scattered fields. Pt I: Waveforms and the general process; Pt 11: Moments. Spectra and special distributions; Pt 111: Waveforms and fields; Pt IV: Statistical models," IEEE Trans. Inform. Theory, vol. IT-13. no. 3, Pt I: pp. 372-392, Pt 11: pp. 393-414, July 1967; vol. IT-18, no. 1, Pt 111: pp. 35- 67, Pt IV: pp. 68-90, Jan. 1972
- [8]. R. L. Mitchell & D.A. McPherson, "Generating nonstationary random sequences," IEEE Transaction Aerospace Electronic System Vol. AES, July 1981 pp-553-560.